

Impact Force Reconstruction of Composite materials based on Improved Regularization Technology

Yajie Sun^{1,2,3*}, Tao Yin¹, Jian Yang¹, Zhiyu Cai¹ and Shaoen Wu⁴

¹ School of Computer & Software, Nanjing University of Information Science & Technology, Nanjing, China

² Engineering Research Center of Digital Forensics, Ministry of Education, Nanjing University of Information Science & Technology, Nanjing, China

³ Jiangsu engineering Centre of Network Monitoring, Nanjing University of Information Science & Technology, Nanjing, China

⁴ Department of Computer Science, Ball State University, Muncie, USA

[E-mail: yanacn@163.com, 2045945879@qq.com, 1477178778@qq.com, 1037347598@qq.com, swu1235@ilstu.edu]

*Corresponding author: Yajie Sun

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Abstract

In the structural health monitoring of composite materials, in order to solve the ill-posed problem of impact force reconstruction, regularization techniques are often used to deal with it. Due to the poor convergence of the traditional Tikhonov regularization method, in order to accurately reconstruct the time history of the impact force, this paper improves Tikhonov regularization method and constructs homotopy function with strong convergence. Since the optimal regularization parameters need to be found in the homotopy function, the Newton downhill method is used to find the optimal parameters and the homotopy function can be calculated, which can accurately reconstruct the time history of the impact force. In order to verify the universality of the method in this paper, impact hammers of different materials were used in the experiment in this paper to study and compare the reconstruction effect of impact time history of different impact hammers.

Keywords: Impact damage, composite materials, impact force reconstruction, improve regularization method.

1. Introduction

In the actual service life of large mechanical equipment, a variety of structural damage often occurs under the action of various external forces, which damages its mechanical strength and ultimately leads to disastrous consequences [1-2]. Composite materials have outstanding potential and advantages in spacecraft manufacturing, the exploration of structural failures caused by external low-velocity shocks is very important for aerospace structures because these structures are often subjected to external forces during manufacture and operation. Accidental effects such as low-speed impacts from various external sources, including birds, hail, runway debris, fall tools, etc., can lead to serious damage, resulting in a decrease in stiffness, integrity and strength of the lightweight composite structure. Low-speed lateral impact can cause different types of damage, such as delamination of carbon fiber/epoxy laminate surfaces, matrix cracking, and fiber breakage in composite structures [3-4]. Therefore, the real-time monitoring of the impact force on the composite material is of great significance to judge the damage situation of the composite material and estimate the residual strength of the composite material [5]. By determining the position, direction and strength of the impact force, we can achieve a comprehensive understanding of the impact on the composite structure, and improve the structure design based on this. Mathematically, impact force recognition is an inverse problem [6-7].

The regularization methods for solving inverse problems have been widely used [8-9], including truncated singular decomposition, Tikhonov iteration, and basis function expansion [10-11]. Iterative regularization algorithms such as Landweber and conjugate gradient iterative regularization algorithm are different from the truncated singular value decomposition Tikhonov regularization method. There is no advantage of transferring matrix inversion and no need to clarify regularization parameters. The iterative process is regularized. The process is widely used in inverse problem solving but rarely used in force recognition. Wang Linjun [12] used the improved Tikhonov regularization method to identify different types of dynamic loads. The simulation example shows that it is superior to the Tikhonov regularization method.

Qiu et al. [13] used the time reversal method to study the identification of impact sources in a finite isotropic plate. For a given force position, it is found that the maximum peak of the reconstructed signal occurs at the impact location. Chen et al. [14] used the time reversal method to conduct experimental research on impact force recognition. In the experimental verification, a square aluminum plate with a piezoelectric sensor was used. The results show that the TR method eliminates the near-real-time monitoring of the ill-posedness and structure of the inverse problem. S. Atobe et al. [15] presented a method to identify impact force location and force history without using analytical model.

Kalhor H et al. [16-17] used the inverse algorithm to solve the impact damage problem of materials, Chein-Shan Liu and Chung-Lun Kuo [18] give a dynamical Tikhonov regularization method for solving nonlinear ill-posed problems and Li Jian et al. [19] gave a dynamical Newton-like method with adaptive step size for solving nonlinear algebraic equation, which provided a good foundation for this paper. Mustapha S et al. [20-21] studied the correlation coefficient between the original time reversal signal and the reconstruction time reversal signal to define the damage index of each sensing path, which is then used to identify multiple debonding during the fusion process.

In addition, the ill-conditioned problem of the inverse algorithm is also the focus of scholars at home and abroad. Rezghi M et al. [22] continued to improve and optimize the Tikhonov regularization algorithm for ill-conditioned problems. Chein-Shan Liu et al. [23] also gave a new regularization method to solve ill-posed linear systems. In the actual Lamb wave signal

processing, the spatial resolution of the signal is an important factor affecting the resolution and precision of damage detection. In reference [24], the author proposed a signal domain transform method to transform the original dispersive Lamb wave signal from the time domain to the distance domain. The time-distance transformation on the excitation waveform was specially modified, and the spatial resolution of the signal was effectively improved. The team [25] also reconstructed a new linear dispersion signal from the original Lamb wave signal for dispersion compensation, and at the same time, the group velocity at the center frequency was reduced exponentially, so that the reconstructed signal could obtain good spatial resolution.

In the process of image denoising, Jianwei Zhang et al. [26] put forward an adaptive regularization parameter function based on the gradient and variance of the image, this method has good effect on edge and data denoising. Linjun Wang et al. [27] optimized the regularization method and applied it to practical engineering problems, which has a remarkable effect on solving dynamic force problems.

In this paper, the homotopy method constructor is selected and then the optimal solution is found by Newton's downhill method, and the homotopy function is obtained. The homotopy method has the advantages of universal validity, convergence and flexibility, and has good effects in image reconstruction. Therefore, it is applied to reconstruct the impact force time history. The Newton's downhill method not only has the advantage of Newton's iterative method, but also prevents the Newton's iterative method from being limited by the initial value selection. Therefore, this chapter uses Newton's downhill method to approximate the minimum value and find the optimal parameters. In the homotopy function, the optimal solution of regularization is obtained, that is, the optimal impact force size.

In this study, the first chapter describes the development of research methods in this direction. The second part of this paper, we introduce the related work of deconvolution and the traditional regularization method. The third part introduces the theory of the improved regularization method proposed in this paper. The fourth chapter summarizes the experimental equipment and summarizes the experimental process. The fifth chapter verifies the feasibility and accuracy of the method, and analyzes the experimental results.

2. Previous Work

2.1 Deconvolution

In general, the impact identification problem is non-linear because the expression involving system input, namely, the impact force and the system output, which is a function of unknown parameters [28]. For a better understanding, consider the material on which the force is applied. If the position of the applied force changes, the deflection of each point of the material will also change. Therefore, the identification of the impact location generally takes precedence over the estimation of the time history of the impact force.

In the vibration response of the linear system, for example, the dynamic strain ε recorded at the point α caused by the impact force f applied at the position β can be expressed by the convolution integral as:

$$\varepsilon(\beta, t) = \int_0^t k(\alpha, \beta, t - \tau) f(\alpha, \tau) d\tau \quad (1)$$

Where, the transfer function $k(\alpha, \beta, t - \tau)$ is defined as an impulse response function at the point β at which the impact force is applied at the point α at time $t = \tau$. The discrete form of convolution integral ($t_i = i\Delta t; i = 1, \dots, p$, where p is the number of samples) can be

represented by a Riemann approximation and written as a system of algebraic equations such as:

$$kf = \varepsilon, k \in R^{m \times n}, f \in R^n, \varepsilon \in R^m \quad (2)$$

Where, in the case of $m = n$, the transfer function k is a lower triangular matrix, and $R^{m \times n}$ represents a space having m rows and n columns.

In order to obtain f , equation (2) should be solved inversely to the established transfer function k and the known response ε . The solution (2) for f is often referred to as deconvolution.

Usually, a simple method such as the standard inverse method, that is, a solution of $f = (k^t k)^{-1} k^t \varepsilon$ does not exist or if there is a result that may cause instability. Usually Tikhonov regularization is expressed as:

$$\min \{ \|kf - \varepsilon\|^2 + \lambda \|If\|^2 \} \quad (3)$$

However, the accuracy directly identified by the Tikhonov regularization method is not very high, so an improved regularization method specification must be adopted.

2.2 Traditional Tikhonov regularization method

Among the regularization methods, the Tikhonov regularization method is usually chosen to obtain stable solutions.

$$\min \{ \|\varepsilon - kf\|^2 + \lambda \|If\|^2 \} \quad (4)$$

Where λ is the regularization parameter. Its regular solution is:

$$f_\lambda = (k^* k + \lambda I)^{-1} k^* \varepsilon \quad (5)$$

Where I is the identity matrix, k^* is the conjugate of k . The part of the coefficient matrix at the right end of equation (5) adds the λI term, because this can play a role in overcoming the ill-conditioned matrix of the equation coefficient, so a stable solution can be obtained. Since the regular solution in (5) is related to the parameter λ , the value of λ is different, and the solution is different. Therefore, how to choose the appropriate parameter λ is the key to obtain a stable solution.

The traditional method uses the classical generalized cross validation method to select the appropriate parameter λ . Generalized cross validation is an effective method to select regularization parameter λ .

Cross validation is based on the statistics of the basic ideas, namely, an optimal regularization parameter value should make the model can predict the missing data well, the original data set is divided into training set and test set, firstly, the parameters are obtained by training set, and then the parameters are tested by test set, so that the parameter with the smallest test error is the optimal regularization parameter.

General cross validation depends on the order of data arrangement, while generalized cross validation is invariant for orthogonal transformation of data vectors. The advantage of the generalized cross-validation method is that it does not require prior information about the error norm. Therefore, the choice of the best regularization parameter λ is required to make the GCV function $G(\lambda)$ obtain the minimum value. GCV function G is defined as:

$$G(\lambda) = \frac{\|kf - \varepsilon\|}{(\text{trace}(I - k k_\lambda^I))^2} \quad (6)$$

Where, $f = k_\lambda^I \varepsilon$. Finally, the regularization parameter λ obtained is input into equation (5) to solve the impact force.

3. Proposed Method

3.1 The homotopy function

Because the Tikhonov regularization method has poor noise adaptability, and the L curve sometimes has multiple inflection points, resulting in underestimation [29]. In order to obtain a stable solution, this paper uses the regularization homotopy method. Suppose there are two topological spaces X and Y and two consecutive functions f and g , and f and g are X to Y mappings, if there is a continuous mapping $H:[0:1] X \rightarrow Y$, Satisfied with the following formula:

$$\forall x \in X, H(x, 0) = f(x) \quad \forall x \in X, H(x, 1) = g(x) \quad (8)$$

Then the function f and the function g in the topological space Y are homotopy, and the function H is the path connecting f and g . Therefore, if the equation $f(x) = 0$ is to be solved, the homotopy idea can be used to construct the same function:

$$H(\lambda, x) = (1 - \lambda)f(x) + \lambda g(x) \quad (8)$$

where λ is expressed as a homotopy parameter, and when λ is 0, the equation is $f(x) = 0$. Therefore, in the process of solving the equation, the value of λ is continuously reduced in a certain way, and finally the solution of the original equation can be obtained.

Therefore, according to this homotopy idea, (8) is expressed as:

$$\min = \varphi_\lambda(f) = \{(1 - \lambda)\|kf - \varepsilon\|^2 + \lambda\|f\|^2\} \quad (9)$$

where λ is a regularized homotopy parameter, which satisfies $0 < \lambda < 1$.

In order to minimize (9), the first derivative of λ with respect to f must be zero. Deriving (9) and letting its derivative equal to zero, you get:

$$(1 - \lambda)k^*(kf - \varepsilon) + \lambda f = 0 \quad (10)$$

where the symbol $*$ indicates conjugate transposition. The impact force size can be expressed as:

$$f_\lambda = [(1 - \lambda)k^*k + \lambda]^{-1}(1 - \lambda)k^*\varepsilon \quad (11)$$

3.2 Newton downhill method

Equation (11) is the regular solution of the improved regularization method. For the determination of the regularization parameter λ in the formula, if the optimal regular solution is to be obtained, λ should be gradually approached to zero. First, the Newton method is used to iteratively approach the minimum value. The steps are as follows:

Step 1: Let λ_t be the root of $f_\lambda = 0$, choose λ_0 as the initial approximation of λ_t , pass the point $(\lambda_0, f(\lambda_0))$ as the tangent L of the curve $y = f(\lambda)$, and the equation of L is $y = f(\lambda_0) + f'(\lambda_0)(\lambda - \lambda_0)$, find the intersection of L and x axis. The abscissa $\lambda_1 = \lambda_0 - f(\lambda_0)/f'(\lambda_0)$, said λ_1 is an approximation of λ_0 .

Step 2: Over the point $(\lambda_1, f(\lambda_1))$ to make the tangent of the curve $y = f(\lambda)$, and find the abscissa $\lambda_2 = \lambda_1 - f(\lambda_1)/f'(\lambda_1)$ of the intersection of the tangent and the x-axis, and let λ_2 be the second approximation of λ_t .

Step 3: Repeat the above processes to obtain a sequence of λ_t approximations, where $\lambda_{t+1} = \lambda_t - f(\lambda_t)/f'(\lambda_t)$ is called the $t + 1$ approximation of λ_t , and the above formula is called the Newton iteration formula.

The disadvantage of the Newton method is that its convergence depends on the selection of the initial value. If the initial value is far from the root of the root, the sequence obtained by Newton's method may diverge. To prevent iterative divergence, a condition is added to the

iterative process to make it monotonic:

$$|f(\lambda_{t+1})| < |f(\lambda_t)| \quad (12)$$

Then, the new improved value λ_t is calculated by appropriately weighting the calculation result $\bar{\lambda}_{t+1} = \lambda_t - \frac{f(\lambda_t)}{f'(\lambda_t)}$ of the above Newton method and the approximation $\lambda_{t+1} = \alpha \bar{\lambda}_{t+1} + (1 - \alpha)\lambda_t$ of the previous step, where $\alpha(0 < \alpha \leq 1)$ is the Newton downhill factor. The final calculation result is $\lambda_{t+1} = \lambda_t - \alpha \frac{f(\lambda_t)}{f'(\lambda_t)}$.

When the Newton downhill factor is selected, it is halved from $\alpha = 1$ until the condition of (12) is satisfied. The advantage of using Newton's downhill method is to ensure the parameters can be stably reduced. It also combines the fast convergence of Newton's method to achieve the purpose of this paper.

In this paper, the homotopy regularization parameters are defined between $[0, 1]$. Therefore, the initial value of the regularization parameter is set to 1, and then iteratively descends according to the Newton downhill iteration formula until it gradually approaches zero, and gets the most excellent regularization parameter.

4. Experimental setup and process

As shown in **Fig. 1**, the experimental equipment for the impact experiment of epoxy composite plate includes LC-01 impact hammer, NI USB-4431 data acquisition card, charge amplifier YE5852 and PZT sensor.



Fig. 1. Experimental set-up

Fig. 2 is a schematic diagram of the data acquisition system. The experimental system is divided into two parts: the hardware part and the software part. The hardware part includes data acquisition card, impact hammer containing IEPE (IEPE refers to a kind of acceleration sensor with power amplifier or voltage amplifier), charge amplifier, etc. The software includes

Labview data acquisition system and MATLAB signal processing software.

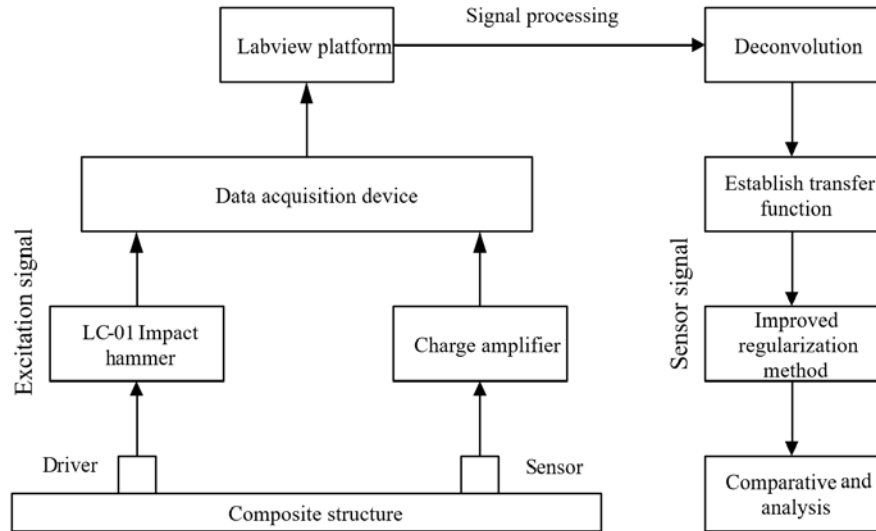


Fig. 2. Experimental process diagram

In the experiment, the PZT sensor and the impact hammer with built-in IEPE sensor were selected as the sensing element, and the NI USB-4431 data acquisition card was combined with the Labview software system to collect the impact signal caused by the impact hammer and simultaneously collect the vibration plate of the composite material plate. Since the output signal of the PZT sensor is very weak, a charge amplifier needs to be placed before receiving the piezoelectric sensing signal, the response signal to be acquired is amplified and converted in advance, and the response signal is collected by the data acquisition card. Since the data acquisition card can save the acquired impact signal and corresponding signal, the acquired signal can be processed and analyzed by MATLAB. Through the deconvolution, the transfer function is established, and then the regularization method is used to solve the ill-posed problem, and the optimal regular solution is obtained. Finally, the validity of the method is proved by comparing the error with the original impact force.

5. Experimental Results and Analysis

5.1 Improved regularization method to reconstruct the impact force time history

The criterion for judging the merits of the regularization parameter is whether the regularization parameter is infinitely approximately zero. As shown in **Fig. 3**, compared with the parameter of the traditional method, the improved regularization parameter is infinitely close to zero. **Fig. 4** shows the time history comparison of the reconstructed impact force using the proposed method, the reconstructed impact force using the traditional method and the actual impact force. The experimental results show that the improved method reduces the noise interference to the experiment and is more stable. The improved impact force time history almost overlaps with the actual impact force time history. The actual impact force is 51.23N, and the improved impact force is 50.456N. Although the impact force of the traditional reconstruction method has little difference in size, the time history of reconstruction has a large deviation.

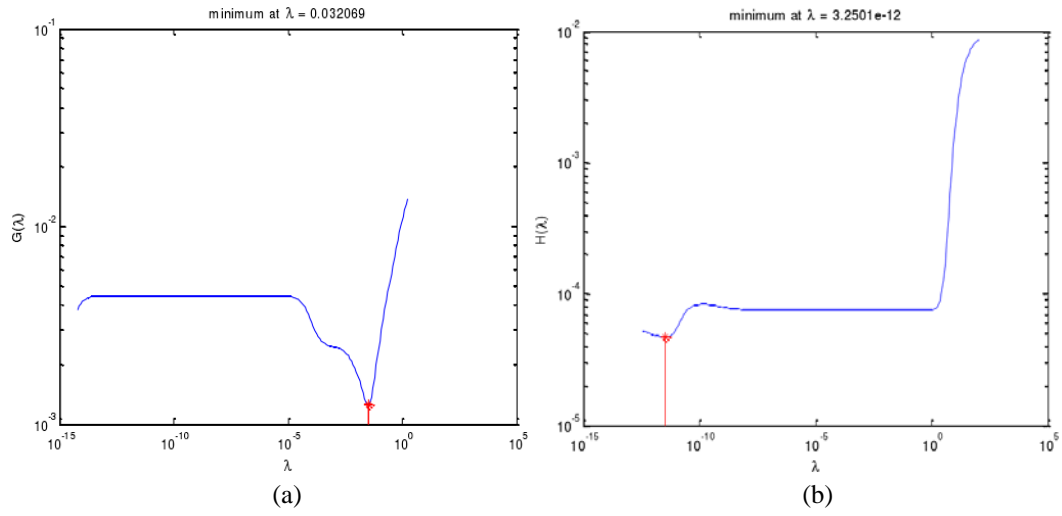


Fig. 3. Comparison of regularization parameters of two methods (a) Traditional regularization method, (b) Improved regularization method

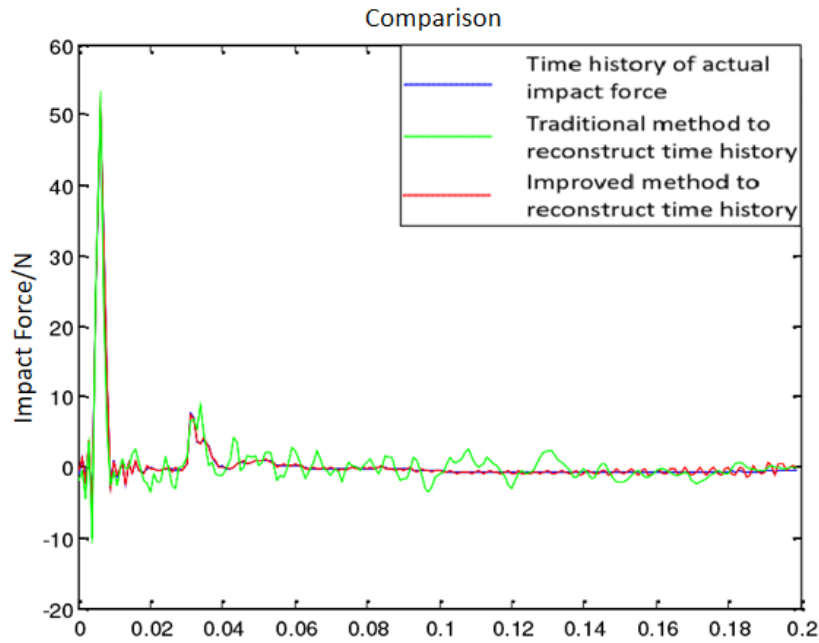


Fig. 4. Comparison of the time history between the two reconstruction methods and the actual impact force

In order to show the effectiveness of the proposed method, the absolute error δ and the relative error Δ are calculated separately.

$$\delta = |f_1 - f| \quad (12)$$

$$\Delta = \frac{|f_1 - f|}{f} \times 100\% \quad (13)$$

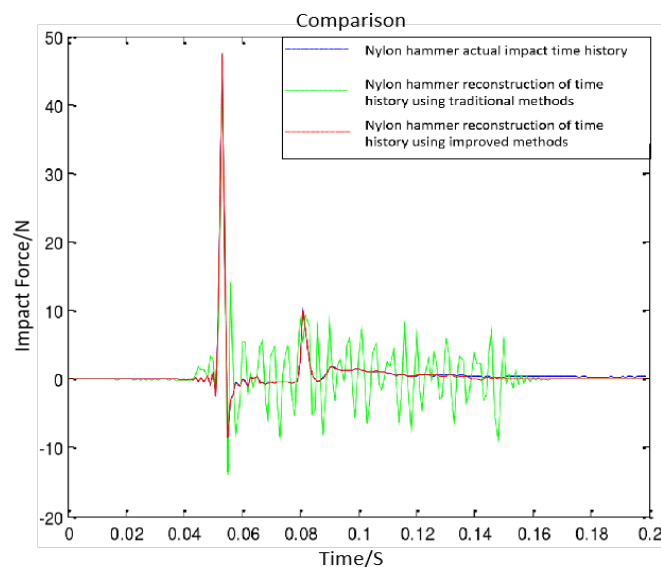
Table 1. The regularization parameters of the time history reconstruction of impact force by the two methods and the error comparison

Class	Regularization parameter	Absolute error (N)	Relative error
The traditional method to reconstruct time history	0.032069	8.9543	0.1336
The improved method to reconstruct time history	0.000020	0.9774	0.0146

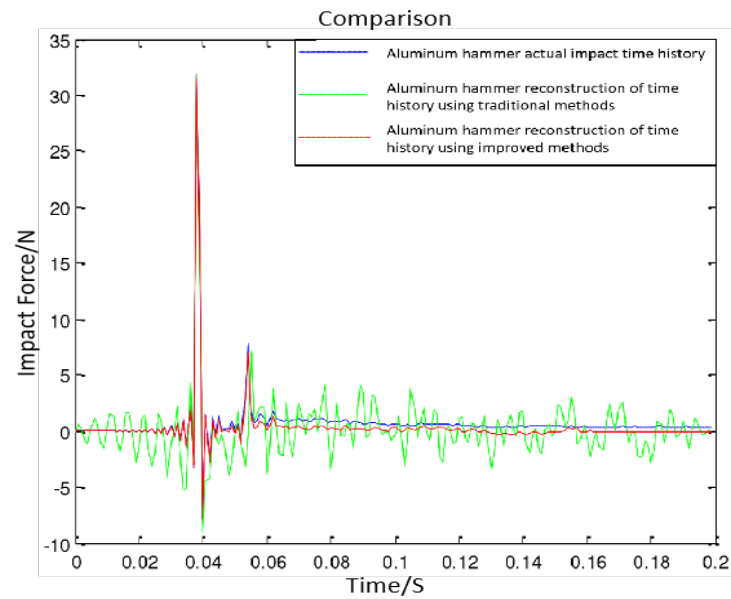
The parameter comparison and error comparison of the recognition results are shown in **Table 1**. The regularization parameter of the traditional method is about 0.032, while the improved regularization parameter is about 0.00002. The absolute error of the traditional method is 8.9N, while the improved method has an absolute error of 8.9N. The absolute error is 0.97N, and the relative error in the final comparison is 0.133 in the traditional method, and only 0.01 in the improved method. Therefore, the improved method can get better applications.

5.2 Reconstruction of impact force time history with different impact hammers

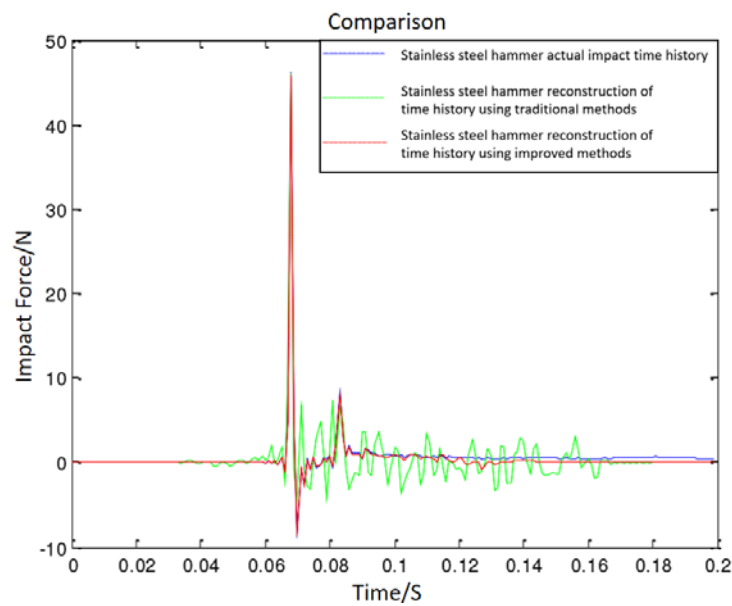
The impact force on the composite plate is very sensitive to the location of the impact and the material properties of the impactor. This experiment uses different impact hammers to reconstruct the impact force time history (nylon hammer, aluminum hammer and stainless steel hammer). In **Fig 5**, from the overall comparison, it can be seen that the reconstruction results of different impact hammer improvement methods are better than the traditional method of impact force reconstruction results, and the error is very small. The results of the regularization parameters, absolute error and relative error of the three different impact hammers are shown in **Table 2**. The regularization parameters of each impact hammer improved method are close to zero, which is much smaller than the regularization parameters of the traditional reconstruction method. Moreover, the absolute error and relative error of the improved method are much smaller than that of the traditional reconstruction method. Therefore, the improved method of reconstructing the impact force time history in this paper is suitable for impact hammers of different stiffness.



(a)



(b)



(c)

Fig. 5. Comparison of time history between impact force and actual impact force of different impact hammers reconstructed by two methods

(a) nylon hammer (b) aluminum hammer (c) stainless steel hammer

Table 2. Two methods to reconstruct the regularization parameters and error comparison of the impact load time history of different impact hammers

Class	Regularization parameter	Absolute error (N)	Relative error
The traditional method to reconstruct the impact time history of nylon hammer	0.058922	11.8956	0.3136
The improved method to reconstruct the impact time history of nylon hammer	0.000342	0.4837	0.0090
The traditional method to reconstruct the impact time history of aluminum hammer	0.344553	7.9959	0.1642
The improved method to reconstruct the impact time history of aluminum hammer	0.000454	1.1980	0.0246
The traditional method to reconstruct the impact time history of stainless steel hammer	0.323768	7.8845	0.2006
The improved method to reconstruct the impact time history of stainless steel hammer	0.000442	0.8445	0.0215

6. Conclusion

This paper introduces the regularization method for solving the ill-posed problem, and studies the advantages of the optimized regularization method for the time history reconstruction of the impact force. Firstly, the homotopy idea is introduced to the Tikhonov method, and the homotopy function is constructed. The Newton downhill method can be used to find the regularization parameter closest to zero, which is used for the homotopy function to obtain the optimal solution and accurately reconstruct the time history of the impact force. Under the same conditions, the time history and regularization parameters of the impact force were reconstructed by comparative experiments and unoptimized methods. Experiments show that with the optimization method, the time history accuracy of impact force reconstruction is significantly improved.

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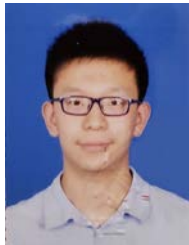
Yajie Sun is currently an associate professor in Nanjing University of Information Science and Technology, Nanjing, China. She received Ph.D. degree in test measurement technology and instrument engineering from Nanjing University of Aeronautics and Astronautics. Her research interests include structural health monitoring, signal processing and big data.



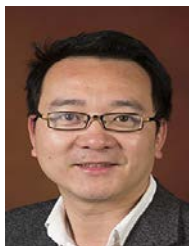
Tao Yin received the B.S. degree in internet of things engineering from Nanjing University of Information Science and Technology, China, in 2019. He is now pursuing a M.S. degree in software engineering at Nanjing University of Information Science & Technology, Nanjing, JiangSu, China. His research interest is composite material structure health monitoring.



Jian Yang received the B.S. degree in Electronic Information Engineering from Jiangsu Ocean University, China, in 2019. He is now pursuing a M.S. degree in software engineering at Nanjing University of Information Science & Technology, Nanjing, JiangSu, China. His research interest is composite material structure health monitoring.



Zhiyu Cai, currently studying as an undergraduate at Nanjing University of Information Science & Technology, is now majoring in information security. His research interest is Deep learning convolutional neural network.



Shaoen Wu received his PhD degree in Computer Science and Software Engineering from Auburn University. He serves on the Advisory Council of Scholarship for the Vice Provost for Research, and the Dean's Faculty Advisory Board. He is a senior member of IEEE, the secretary of IEEE MMTC 2018-2020, and a member of ACM. He has published over 70 peer-reviewed papers in wireless, IoT, smart health and robotics at international journals e.g. IEEE Internet of Things Journal and conferences e.g. IEEE Globecom, ICC and ICCCN.